

## REMARKS

By this amendment, applicants have provided a substitute specification accompanied by another, separate version of the substitute specification, marked up to show all of the changes relative to the previous version of the specification. The substitute specification is an English translation of the international publication, originally published in French. The English translation originally provided was inadvertently an English translation of the French priority text, not of the international application. The substitute specification correctly provides an English translation of the international publication. Therefore, the substitute specification contains no new matter in relation to the international application.

Applicants have also amended the claims to more clearly define their invention. In particular, claim 3 has been amended to be in independent form (based on the claims in the international application). In particular, it is noted that claim 3 recites that the at least one non-ionic amphiphilic compound is obtained by reaction of at least one polymerized vegetable oil having a viscosity ranging between 5 and 60 Pa.s at 20°C or at least fatty acid on at least one aminoalcohol; the phrase "or at least one fatty acid" appeared in original claim 1 of the international application. Claim 1 has been canceled without prejudice or disclaimer and the remaining claims amended to ultimately depend from claim 3 and to be consistent therewith. Claims 6, 7, 10 and 12 have been amended to eliminate the indefiniteness problems noted by the Examiner in numbered section 2 of the office action. In all of the amended claims, applicants have amended the phrase "lubricating compound" to read --lubricating composition-- since the lubricating material can be in the form of a mixture, not just a compound.

It is noted that the substitute specification includes an English translation of the claims in the international application. On the other hand, by the foregoing amendments, applicants have amended the claims as they appear in the English translation originally provided.

In view of the foregoing amendments, it is submitted all of the claims now in the application comply with the requirements of 35 USC 112, second paragraph. Therefore, reconsideration and withdrawal of the rejection of claims 6, 7, 10 and 12 under 35 USC 112, second paragraph, are requested.

In view of the cancellation of claim 1 and the amendments amending the remaining claims to ultimately depend from claim 3, it is submitted the rejection of claims 1, 2, 4 - 9 and 11 under 35 USC 102(b) in numbered section 4 of the office action and the rejection of claims 1, 4, 5, 6 and 11 under 35 USC 102(b) in numbered section 5 of the office action are moot.

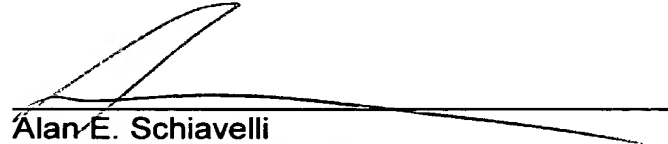
Applicant notes that claim 3 would be allowable if rewritten in independent form. It is noted that claim 3 has been rewritten in independent form, albeit with the addition of the phrase "or at least one fatty acid"; it is submitted all of the claims now in the application are now in condition for allowance.

To the extent necessary, applicants petition for an extension of time under 37 CFR 1.136. Please charge any shortage in the fees due in connection with the filing of this paper, including extension of time fees, to the deposit account of Antonelli, Terry, Stout & Kraus, LLP, Deposit Account No. 01-2135 (Case: 612.39321X00), and please

credit any excess fees to such deposit account.

Respectfully submitted,

ANTONELLI, TERRY, STOUT & KRAUS, LLP



Alan E. Schiavelli  
Registration No. 32,087

AES/jla  
(703) 312-6600

VERSION WITH MARKINGS TO SHOW CHANGES

IN THE CLAIMS:

2. (Amended) A fluid as claimed in claim-~~43~~, characterized in that said at least one polymerized vegetable oil or said at least one fatty acid is selected from the group consisting of linseed, safflower, grapeseed, wood, sunflower oil, ~~or~~ mixtures thereof, and a fatty acid derived therefrom.
3. (Amended) A water-base well fluid ~~as claimed in claim 1~~, characterized in that ~~said comprising a lubricating composition containing at least one non-ionic amphiphilic compound obtained by reaction of at least one polymerized~~ vegetable oil ~~is polymerized and has~~ having a viscosity ranging between 5 and 60 Pa.s at 20°C or at least one fatty acid on at least one aminoalcohol.
4. (Amended) A fluid as claimed in claim-~~43~~, characterized in that said aminoalcohol is diethanolamine.
5. (Amended) A fluid as claimed in claim-~~43~~, characterized in that the lubricating ~~compound~~ composition is conditioned in form of a mixture comprising at least one solvent.
6. (Amended) A fluid as claimed in claim 5, characterized in that said solvent is a vegetable oil derivative selected from the group consisting of C6 to C18 fatty acid esters and C2 to C18 linear or branched alcohol esters.
7. (Amended) A fluid as claimed in claim 5, characterized in that said mixture contains between 0 and 80% by mass of solvent ~~and preferably between 20 and 40%.~~

8. (Amended) A fluid as claimed in claim-~~13~~3, characterized in that it comprises a concentration of 0.1 to 5% by weight of said lubricating-~~compound~~ composition.

10. (Amended) A fluid as claimed in claim-~~13~~3, characterized in that its pH value is above 9, ~~and preferably above 10~~.

12. (Amended) Application of the process as claimed in claim 11 to well fluids with a pH value above 9 ~~and preferably above 10~~.



**WELL FLUID COMPRISING A LUBRICATING COMPOSITION - PROCESS  
FOR CONTROLLING THE LUBRICATION OF A WELL FLUID -  
APPLICATION TO HIGH-PH FLUIDS**

**FIELD OF THE INVENTION**

5       The present invention relates to fluids used for drilling, well completion or workover in wells. More particularly, the invention describes a water-base fluid comprising a lubricating compound, and a process for controlling the lubricating power of water-base fluids placed in boreholes. In an application, the water-base well fluids have a pH value above 9.

10

**BACKGROUND OF THE INVENTION**

      The conventional method for drilling wells, petroleum wells or not, consists in driving in rotation a toothed bit fastened to the end of a drillpipe string, the string being generally driven in rotation by a surface installation. A fluid, referred to as drilling fluid or mud, is injected in the vicinity of the bit through the inner space of the drillpipes. The  
15   main functions of this fluid are to clean the bit and the well by driving the debris towards the surface, to stabilize the walls of the well, to inhibit reactions of geologic formations in contact with the fluid, etc.

      The present invention does not only relate to fluids referred to as drilling fluids, but also to fluids referred to as completion fluids and to fluids referred to as workover  
20   fluids. Completion is an operation which continues the drilling operation when the well reaches the producing formation. Completion notably consists in drilling into the reservoir rock, testing the formation, equipping the well for production, bringing in the

well. For these operations, the completion fluid can be specific notably to the reservoir rock and to the effluents produced. Workover operations consist in working in a producing well in order to drill, redrill, clean the well, or change well equipments.

Well fluids must have adjusted characteristics according to various uses, notably  
 5 their viscosity, their density or their filtrate control capacity. In the case of greatly deflected wells, horizontal wellbores for example, or more generally wells leading to extensive friction on the tubulars lowered in the well, the lubricating capacity of the fluid becomes an important characteristic.

High-pH fluids are sometimes used, i.e. above 9 and generally above about 10, for  
 10 example silicate-base drilling muds such as those described in the SPE 37,266 publication presented at the « International Symposium on Oilfield Chemistry, 18-21 February 1997, Houston TX ». These muds are recently used notably for their qualities as regards swelling inhibition of the clays drilled.

#### SUMMARY OF THE INVENTION

15 The present invention thus relates to a water-base well fluid comprising a lubricating compound containing at least one non-ionic amphiphilic compound obtained by reaction of at least one vegetable oil or one fatty acid on at least one aminoalcohol.

All the vegetable oils or vegetable fatty acids are suitable. The vegetable oil or fatty acid can be selected from the group consisting of linseed, safflower, grapeseed, wood,  
 20 sunflower, rapeseed oil, or mixtures thereof, or of a fatty acid derived from these vegetable oils.

In a variant, the vegetable oil or fatty acid can be polymerized and have a viscosity ranging between 5 and 60 Pa.s at 20°C after polymerization.

The aminoalcohol used can be diethanolamine.

The lubricating compound can be conditioned in form of a mixture comprising one  
5 or more solvents and possibly other compounds.

The solvent of the mixture can be a vegetable oil derivative.

The mixture (lubricating compound and solvents) can contain between 0 and 80 %  
by mass of solvent and preferably between 20 and 40 %.

The well fluid can comprise a concentration of 0.1 to 5 % by weight of the  
10 lubricating compound, preferably ranging between 0.5 and 2 % by weight.

The fluid according to the invention can have a pH value above 9, preferably above  
10.

The invention also relates to a process for controlling the lubricating power of a  
water-base well fluid which consists in incorporating to the fluid a lubricating  
15 compound as defined above.

The invention comprises an application of the process above to well fluids having a  
pH value above 9 and preferably above 10.

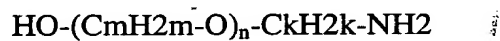
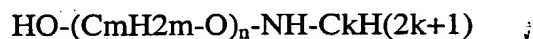
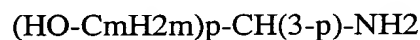
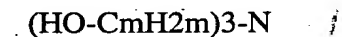
Although all the vegetable oils or vegetable fatty acids can be suitable, greatly  
unsaturated oils are preferably used, such as linseed, safflower, grapeseed, wood,  
20 sunflower oil, or mixtures thereof. These vegetable oils or fatty acids are used as they  
are or polymerized. Polymerized vegetable oils (stand oils) are obtained by thermal



treatment of the aforementioned greatly unsaturated vegetable oils, under such conditions that there is no oxidation. Linseed oil or fatty acid (preferably refined) is generally used, but it is also possible to use safflower, grapeseed, wood, sunflower oil or of fatty acid, or mixtures thereof. In order to prepare the lubricating compound according to a variant of the invention, a polymerized vegetable oil or fatty acid having a viscosity ranging between 5 and 60 Pa.s at 20°C can be used. By way of example, the thermal treatment of a refined linseed oil at a temperature of 290-300°C yields, after 6 to 12 hours, a product having a viscosity of 10 Pa.s at 25°C.

The aminoalcohols used to prepare the compounds of the invention are amines or polyamines comprising one or more alcohol groups and possibly one or more ether groups.

For example, the aminoalcohols can correspond to the following formulas :



with  $m=2$  to  $6$  ;  $k=1$  to  $6$  ;  $p=2$  or  $3$  ;  $n=2$  to  $20$

One can mention in particular :

monoethanolamine :  $\text{OH}-(\text{CH}_2)_2-\text{NH}_2$ ,

monopropanolamine :  $\text{OH}-(\text{CH}_2)_3-\text{NH}_2$ ,

monoisopropanolamine :  $\text{CH}_3-\text{CH}(\text{OH})-\text{CH}_2-\text{NH}_2$ ,

2-amino-1-butanol :  $\text{CH}_3-\text{CH}_2-\text{CH}(\text{NH}_2)-\text{CH}_2-\text{OH}$ ,

5 1-amino-2-butanol :  $\text{CH}_3-\text{CH}_2-\text{CH}(\text{OH})-\text{CH}_2-\text{NH}_2$ ,

N-methyl-ethanolamine :  $\text{CH}_3-\text{NH}-(\text{CH}_2)_2-\text{OH}$ ,

N-butyl-ethanolamine :  $\text{CH}_3-(\text{CH}_2)_3-\text{NH}-(\text{CH}_2)_2-\text{OH}$ ,

pentanolamine, hexanolamine, cyclohexanolamine, polyalkanolamines or  
polyalkoxyglycolamines, with the following formula :

10  $\text{OH}-(\text{CH}_2-\text{CH}_2-\text{O})_n-\text{CH}_2-\text{CH}_2-\text{NH}_2$  (n between 1 and 30),

and aminopolyols such as :

diethalonamine :  $(\text{OH}-\text{CH}_2-\text{CH}_2)_2-\text{NH}$ ,

diisopropanolamine :  $(\text{CH}_3-\text{CH}(\text{OH})-\text{CH}_2)_2-\text{NH}$ , or

trihydroxymethylaminomethane :  $((\text{HO})\text{H}_2\text{C}-)_3\text{C}-\text{NH}_2$ .

15 The synthesis of the compounds of the invention can be obtained by reacting excess aminoalcohol, preferably diethanolamine, on a vegetable oil or a vegetable fatty acid as it is, or polymerized, preferably obtained from linseed oil.

The reaction is preferably carried out in the absence of solvent, generally at a temperature above about  $100^\circ\text{C}$ , and preferably ranging between  $100$  and  $200^\circ\text{C}$ .

20 However, if the viscosity of the reaction medium is too high, the reaction can be carried out in the presence of a solvent.

The lubricating compound included in the fluid according to the invention is obtained at the end of the reaction.

This compound can be incorporated to the high-pH aqueous well fluid as it is or not, or in form of a mixture comprising a solvent or several solvents and possibly other  
5 compounds.

In order to obtain a mixture having an acceptable viscosity, considering the applications envisaged, a solvent can be added. A certain number of solvents can be used, in particular aromatic cuts ; however, all the solvents derived from natural oils are preferably used, such as C6 to C18 fatty acid esters and C2 to C18 linear or branched  
10 alcohol esters, in order to obtain a biodegradable and non-polluting additives solution.

When used as lubricating additives for a well fluid, these compounds are added to the well fluid at concentrations generally ranging from 0.1 to 5 % by mass, preferably from 0.5 to 2 % by mass.

It can be noted that the regulations relative to environmental protection increasingly  
15 require the use of non-toxic and non-polluting additives in the formulation of well fluids.

The well fluid according to the present invention comprising the lubricating composition notably has the advantage of meeting the current criteria relative to environmental protection.

20 Furthermore, the present composition can be used with all the high-pH water-base well fluids, for example, silicate-base fluids, weighted or not, certain high-pressure/high temperature (HP/HT) fluids, etc.

High pH values are difficult conditions for the stability of lubricating products, in particular those based on conventional esters which hydrolyze at a high pH value and under the effect of the temperature.

#### DETAILED DESCRIPTION

5 Other features and advantages of the invention will be clear from reading the description hereafter of non limitative examples.

The lubricating power of a lubricating composition added to a well fluid according to the invention is tested by means of a « Lubricity tester-Model 212 » manufactured by the NL Baroid Petroleum Services company (Instruction Manual Part  
10 No.211210001EA). The tests (« Lubricity-surface to surface ») are carried out according to the procedures recommended by the RP 13B standard of the American Petroleum Institute (API) (100 psi (689 kPa) at 60 rpm). In order to compare the lubricating capacities of various compositions, the graduations obtained with the testing device described above were read. These readings correspond to relative values of the  
15 friction torque. The lower these values, the higher the lubricating power of the composition tested.

The principle of the examples given hereafter is to mix with a base fluid a certain amount of a determined lubricating composition, the mixture being then tested in the device. The tests, unless otherwise indicated, were carried out at ambient temperature  
20 (about 25°C).

A first lubricating composition, given by way of example, and added to the base well fluid, is referred to as NTL.

NTL is the result of the reaction of 52 kg polymerized linseed oil having a viscosity of 10 Pa.s with 28 kg diethanolamine, in a 100-litre reactor, heated for one hour at 160°C. Its viscosity is of the order of 2700 mPa.s at 40°C.

A second lubricating composition, referred to as XTL, is the product of the reaction of 52 kg linseed oil with 28 kg diethanolamine in the same reactor as above and under the same conditions.

Example 1 : Silicate mud before aging

Composition of the base fluid :

	-	fresh water	
10	-	viscosifier (xanthan)	5.2 g/l
	-	filtrate reducer (Aquapac-Regular)	0.14 g/l
	-	filtrate reducer (Aquapac-LV)	2.51 g/l
	-	filler clay	20 g/l
	-	sodium silicate	84.7 g/l
15	-	sodium chloride	50 g/l
	-	barite	93 g/l
	-	NaOH in order to obtain :	pH=11.

The xanthan used for all the tests is IDVIS marketed by the Dowell Drilling Fluids company.

20 The CMC AQUAPAC Regular and LV type products are marketed by the Aqualon company.

This test shows the lubricating power of the lubricant NTL added to a high-pH base fluid according to the concentration by weight.

Lubricant NTL (%)	Torque reading	
	(lbs.in)	N.m
0	42	4.75
0.5	25	2.8
1	23	2.6
1.5	21	2.4
2	17	1.9
3	17	1.9
4	17	1.9
5	17	1.9

A decrease in the value of the torque can be observed as the lubricant concentration increases. The results show the good performances of the NTL system with this high-pH formulation. A lubricating additive concentration of the order of 2 % is optimum here.

#### Example 2 : Silicate mud after aging

The formulation of the previous base fluid is used, mixed with 2 % NTL that has been aged in a « Hot Rolling » test cell at 80°C for 16 hours, then return to ambient temperature. The following results show that temperature aging does not degrade the lubricating properties of the NTL additive in a high-pH mud.

	Torque reading	
	(lbs.in)	(N.m)
Before aging	17	1.9
After aging	18	2.03

Example 3 : Influence of the lubricant on the rheological and filtering properties of the mud

The rheological properties of the mud are expressed hereafter in VA, apparent viscosity, in centipoise (cP), VP, plastic viscosity, in centipoise (cP), YV is the yield value in lb/100 ft<sup>2</sup> and gel 0 and gel 10 (these measurements are in accordance with the API RP 13B1 standard which gives the correspondences of the SI units in Appendix I),  
 5 with and without NTL, before (AV) and after (AP) 16-hour aging at 80°C, as well as the filtering properties expressed by the corrected amount of filtrate (in cm<sup>3</sup>) obtained after 30-minute filtration.

The formulation of the base fluid is the same as that of the silicate mud in example 1.

	without NTL (AV)	with 2 % NTL (AV)	without NTL (AP)	with 2 % NTL (AP)
VA	34	41	32	43
VP	11	20	17	22
YV	46	42	30	42
Gel 0 / Gel 10	11/15	5/8	8/10	8/15
Filtrate (ml)	2.6	2.0	4.6	3.9

10 These results show that addition of the optimized percentage of NTL does not significantly modify the rheological and filtering properties of the mud, whether before or after aging.

#### Example 4 : Dilution of NTL by a solvent

Various lubricating compounds were tested (L1, L2, L3, L4, L5, L6), all  
 15 representative of the present invention. The percentages are expressed by weight. The viscosities measured at 40°C are given in the table hereunder.

Mixtures	Viscosity (mPa.s)
L1 : NTL-100%	2670
L2 : NTL-80% + Methyl oleate-20%	790
L3 : NTL-70% + Methyl oleate-30%	410
L4 : NTL-80% + 2-butyl C12-C14-20%	710
L5 : NTL-70% + 2-butyl C12-C14-30%	385
L6 : NTL-70% + 2-butyl C12-C14-30% + 2-octanol (5% in relation to the 2-butyl C12-C14)	350

The lubricating performances and the characteristics of the various mixtures are given hereafter. The mixtures were added in a proportion of 1 or 2 % by weight to the formulation of silicate mud of example 1.

Before aging

	Concentration	Torque reading		VA	VP	YV
	%	(lbs.in)	(N.m)	mPa.s	mPa.s	lbs/100 ft <sup>2</sup>
L1	2	17	1.9	41	20	42
L2	2	18	2.03	42	19	46
L3	1	24	2.7	34	13	42
L4	1	24	2.7	31	14	34
L4	2	18	2.03	33	15	36
L5	2	20	2.3	40	19	42
L6	2	18	2.03	39	18	42

5

After 16-hour aging at 80°C

	Concentration	Torque reading		VA	VP	YV
	%	(lbs.in)	(N.m)	mPa.s	mPa.s	lbs/100 ft <sup>2</sup>
L1	2	18	2.03	43	22	42
L4	2	19	2.15	34	15	38
L6	2	18	-	39	18	42

These results show the very good performances of the systems studied in terms of lubrication. The main interest of using a diluent is to reduce the viscosity of additive NTL, which facilitates its incorporation to the aqueous fluid.



Example 5 : Silicate mud and compound XTL

The formulation of silicate mud of example 1 is used, before aging and after aging as described in example 2.

Before aging

Lubricant XTL	Torque reading	
	lbs.in	N.m
%		
0	42	4.75
0.5	26	2.9
1	24	2.7
1.5	22	2.5
2	22	2.5
3	22	2.5

5 After aging

Lubricant XTL	Torque reading	
	lbs.in	N.m
%		
2	22	2.5

These results show that lubricating compound XTL allows to significantly decrease frictions. Its characteristics are not altered after aging.

Example 6 : Seawater bentonite mud

Composition of the base fluid :

- 10
- seawater
  - bentonite 30 g/l
  - viscosifier (xanthan) 2 g/l
  - filtrate reducer (Aquapac-LV) 1 g/l
  - dispersant 3 g/l
- 15
- barite, such that the density SG = 1.2 kg/l.

The dispersant used is polyacrylate FP30S marketed by the COATEX company (France).

The pH value of the formulation is adjusted to soda NaOH, so that pH = 9 or pH = 12.

- 5 This test gives the results of the lubricating power of the high-pH fluid according to the concentration of lubricant NTL added.

Lubricant NTL	Torque reading			
	pH 9		pH 12	
%	lbs.in	N.m	lbs.in	N.m
0	36	4.07	36	4.07
0.5	34	3.84	32	3.62
1	31	3.5	21	2.37
2	31	3.5	18	2.04
3	25	2.8	18	2.04
4	21	2.37	18	2.04
5	19	2.15	16	1.81

These results show the very good lubricating performances of NTL, notably at a high pH value.

#### Example 7 : Cesium formate mud

- 10 Composition of the base fluid :

- seawater
- viscosifier (xanthan) 2 g/l
- filtrate reducer 2 g/l
- filling clay 10 g/l
- 15 - KCl 50 g/l

- CsCOOH, H<sub>2</sub>O (hydrated cesium formate) :

300 g/l, so that the density

SG = 1.2 kg/l.

The pH value of the formulation is adjusted to soda NaOH, so that pH = 9 or pH = 12.

This test shows the lubrication results according to the concentration of lubricant NTL added.

Lubricant NTL	Torque reading			
	pH 9		pH 12	
%	lbs.in	N.m	lbs.in	N.m
0	36	4.07	40	4.52
0.5	16	1.81	18	2.04
1	4	0.45	6	0.68
2	2	0.23	2	0.23
3	2	0.23	2	0.23

- 5 These measurements show the very good lubricating performances of NTL in this type of very high-pH fluid.

## CLAIMS

1) A water-base well fluid, characterized in that it comprises a lubricating compound containing at least one non-ionic amphiphilic compound obtained by reaction of at least one vegetable oil or one fatty acid on at least one aminoalcohol.

5        2) A fluid as claimed in claim 1, characterized in that said vegetable oil or fatty acid is selected from the group consisting of linseed, safflower, grapeseed, wood, sunflower, rapeseed oil, or mixtures thereof, or of a fatty acid derived from these vegetable oils.

3) A fluid as claimed in any one of claims 1 and 2, characterized in that said  
10 vegetable oil is polymerized and has a viscosity ranging between 5 and 60 Pa.s at 20°C.

4) A fluid as claimed in any one of claims 1 to 3, characterized in that said aminoalcohol is diethanolamine.

5) A fluid as claimed in any one of claims 1 to 4, characterized in that the lubricating compound is conditioned in form of a mixture comprising at least one  
15 solvent and possibly other compounds.

6) A fluid as claimed in claim 5, characterized in that said solvent is a vegetable oil derivative.

7) A fluid as claimed in any one of claims 5 and 6, characterized in that said mixture contains between 0 and 80 % by mass of solvent and preferably between 20 and  
20 40 %.

8) A fluid as claimed in any one of the previous claims, characterized in that it comprises a concentration of 0.1 to 5 % by weight of said lubricating compound.

9) A fluid as claimed in claim 8, characterized in that said concentration ranges between 0.5 and 2 % by weight.

5        10) A fluid as claimed in any one of the previous claims, characterized in that its pH value is above 9, and preferably above 10.

11) A process for controlling the lubricating power of a water-base well fluid, characterized in that a lubricating compound as claimed in any one of claims 1 to 9 is added to said fluid.

10        12) Application of the process as claimed in claim 11 to well fluids with a pH value above 9 and preferably above 10.